# Location estimation for indoor autonomous vehicle navigation by omni-directional vision using circular landmarks on ceilings ${ }^{\star}$ 

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#### Abstract

A novel approach to location estimation by omni-directional vision for autonomous vehicle navigation in indoor environments using circular landmark information is proposed. A circular-shaped landmark is attached on a ceiling and an omni-directional camera is equipped on a vehicle to take upwardlooking omni-directional images of the landmark. This way of image taking reduces possible landmark shape occlusion and image noise creation, which come from the existence of nearby objects or humans surrounding the vehicle. It is shown that the perspective shape of the circular landmark in the omnidirectional image may be approximated by an ellipse by analytic formulas with good shape-fitting effect and fast computation speed. The parameters of the ellipse are then used for estimating the location of the vehicle with good precision for navigation guidance. Both simulated and real images were tested and good experimental results confirm the feasibility of the proposed approach.


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## 1. Introduction

Location estimation is essential for guidance of autonomous vehicles in many indoor navigation applications. A widely adopted approach is the vision-based technique. Most existing vision-based techniques deal only with frontal scenes acquired by traditional cameras and are easily interfered by unexpected objects around the vehicle. A feasible solution to this problem is to use an omnidirectional camera [1-6] which looks upward at certain target shapes, called landmarks usually, attached on the ceiling [7]. This solution has the unique advantage of providing wide-angle views with fewer objects appearing in the field of view, thus reducing the guidance error coming from landmark occlusion, noise inference, etc. This is important for applications of intelligence robots such as cleaning robots, pet robots, tour guide robots, etc., which must work among humans or objects at close distances. On the other

[^0]hand, even though obtaining the distance and orientation of the circular landmarks on the ceiling can be easily realized with a standard camera [8,9], a well-designed single omni-directional camera system may be used to replace several standard cameras so far as the image taking range is concerned.

In this study, the landmark is selected to be a circle. Analysis of circular shapes in omni-directional images is not well studied so far. It is found in this study that a circular shape, which becomes an irregular shape in an omni-directional image with no known shape descriptor, can be well approximated analytically by an elliptical shape. Consequently, it is appropriate to guide a vehicle equipped with an upward-looking omni-directional camera using a circular shape attached on a ceiling as a landmark, as is done in this study. Several merits can be identified in this approach, including: (1) the circular-shaped landmark attached on the ceiling is identically observable from every direction; (2) the circular shape, being elliptical when imaged, is easier to detect in low-resolution omnidirectional images; (3) the elliptical shape provides more precise parameters for location estimation; (4) the elliptical shape does not get mixed up easily with other shapes found in the environment. Owing to these merits, stable and precise relative vehicle location estimation can be achieved for navigation. An illustration of the experimental navigation environment for this study, including a vehicle, a ceiling, and a landmark, is shown in Fig. 1.

Most vehicle location estimation techniques using omnidirectional images proposed up to now can be grouped into


Fig. 1. Relative positions of camera, ceiling, and circular landmark for providing sufficient field of view and avoiding unexpected objects and humans appearing in acquired images.
three types: triangulation, full-scene matching, and mirror-lens projection, in accordance with the way of image information. In triangulation techniques [1,2], a standard location method is to identify surrounding landmarks in the environment and find their corresponding locations in the environment map built in advance. By the measured bearings of the landmarks [1], the location of an autonomous vehicle can be obtained. Yagi [2] correlated the angle of the vertical edge in an omni-directional image to the environment map to acquire the location of the vehicle. However, sometimes it is difficult to find natural landmarks which can be identified stably from omni-directional images.

In full-scene matching techniques [3,4], a vehicle locates itself by comparing images taken at its current location with reference images stored in its memory. Full-scene matching provides better feasibility by the use of omni-directional cameras. However, it takes much reference memory space to raise location precision. Gasper [3] showed that the position of the vehicle in the environment can be determined by comparing the vehicle's current view with previously learned images, using a lowdimensional subspace of the input images obtained from a principal component analysis process. Menegatti [4] simplified the location problem by using the Fourier components of omnidirectional images as the signatures of the acquired views.

The unique mirror-lens projection relation of the omnidirectional camera also can be used to derive the location of an autonomous vehicle by 3-D computer vision techniques [5,6]. In Koyasu [5], the range information, which is obtained by an omnidirectional stereo vision system composed of a pair of verticallyaligned omni-directional cameras, helps not only creating a 3-D map but also locating the vehicle itself. In [6], Cauchois compared synthetic landmark images with real landmark images taken from a calibrated omni-directional camera to accomplish absolute vehicle location works. However, these methods might be unstable or inapplicable for locating a vehicle in a space crowded with people or full of objects, such as in an exhibition room or in a library.

In the proposed approach, at first an upward-looking omnidirectional camera on a vehicle is used to take an image of a circular-shaped landmark attached on the ceiling of an indoor space. An ellipse detection algorithm [10] is applied next to detect the projected shape of the landmark in the image. The irregular shape formed from the circular shape in the omni-directional image is approximated by an elliptical shape. The location of the landmark, including its distance and orientation, with respect to the camera on the vehicle are then derived analytically in terms of the major axis length and the center coordinates of the approximating ellipse. Finally, the move distance and the orientation change of the vehicle between two consecutive observations of the landmark are derived, which are useful for a number of autonomous vehicle applications.

The remainder of this paper is organized as follows. In Section 2, we derive the analytic equations for approximating as an elliptical shape the irregular shape in an omni-directional image taken of a circular-shaped landmark. In Section 3, we describe how to estimate the vehicle location from the acquired image using the derived analytic equation, and show an application of the results to autonomous vehicle guidance. In Section 4, some experimental results are described to show the precision and feasibility of the proposed method. Finally, some conclusions are given in Section 5.

## 2. Approximation of irregular shape in omni-directional image taken of circular-shaped landmark by ellipse

The circular shape attached on the ceiling of the vehicle navigation environment for use as a landmark becomes irregular with no mathematical shape descriptor in an omni-directional image taken with a hyperboloidal omni-directional camera. We can approximate the irregular shape well by an ellipse, as mentioned previously, and this fact will be proved here. Specifically, an equation of the approximating elliptical shape in the image will be derived. The validity of this ellipse approximation will become clear in the derivation. The precision of the approximation will also be proved by some experimental results.

In Section 2.1, the projection transformation between the camera coordinate system and the image coordinate system will be described first. Then, the coordinate systems will be rotated horizontally to derive the equation of an ellipse in the image. In Section 2.2 a simulated shape of the circular landmark computed with the derived equation will be compared with the shape obtained by an imaging projection based on [5] to show the effectiveness of the proposed elliptical shape approximation.

### 2.1. Approximation of distorted circular shapes in omni-directional images by ellipses

The camera and image coordinate systems involved in this study using a hyperboloidal omni-directional camera are depicted in Fig. 2, with their coordinates specified by $(x, y, z)$, and ( $u, v$ ), respectively. The hyperbolic shape of the omni-directional mirror in the camera coordinate system may be described as:
$\frac{R^{2}}{a^{2}}-\frac{z^{2}}{b^{2}}=-1, \quad R=\sqrt{x^{2}+y^{2}}$.
The focal point $O_{M}$ of the mirror is located at $(0,0,-c)$ and the camera center $O_{c}$ at $(0,0,+c)$, in the camera coordinate system, where $c=\sqrt{a^{2}+b^{2}}$. The projection relationship between the image coordinates $(u, v)$ and the camera coordinates $(x, y, z)$ can be described as follows [5]:

$$
\begin{align*}
& u=\frac{x f\left(b^{2}-c^{2}\right)}{\left(b^{2}+c^{2}\right)(z-c)-2 b c \sqrt{(z-c)^{2}+x^{2}+y^{2}}}, \\
& v=\frac{y f\left(b^{2}-c^{2}\right)}{\left(b^{2}+c^{2}\right)(z-c)-2 b c \sqrt{(z-c)^{2}+x^{2}+y^{2}}}, \tag{2}
\end{align*}
$$

where $f$ is the focal length of the camera.
In Fig. 2, let the circular-shaped landmark and its center and radius be denoted by $W, P_{w}$ and $R_{w}$, respectively. And let the image of $W$ in the hyperboloidal image be denoted by $Q$. Also, let $\left(x_{w}, y_{w}, z_{w}\right)$ denote the camera coordinates of $P_{w}$. In this study, the normal vector of the landmark is assumed to be parallel with the optical axis of the camera. To simplify the derivation described later, we rotate, as shown in Fig. 3, horizontally the camera coordinate system and the image coordinate system through an angle of $\theta_{w}$ defined by:
$\theta_{w}=\tan ^{-1} \frac{y_{w}}{x_{w}}$.


Fig. 2. Coordinate systems involved in this study.


Fig. 3. Top view from the $z$ direction showing the relationship between new and original coordinate system with the new image coordinate system $\left(u^{\prime}, v^{\prime}\right)$ obtained by rotating the $u$-axis through an angle of $\theta_{w}=\tan ^{-1}\left(y_{w} / x_{w}\right)$ with respect to the center of the circular-shaped landmark $W$.

Then, the relation between the original camera coordinates ( $x, y, z$ ) and the resulting ones ( $x^{\prime}, y^{\prime}, z^{\prime}$ ) may be described by:
$x^{\prime}=x \cos \theta_{w}+y \sin \theta_{w}, \quad y^{\prime}=y \cos \theta_{w}-x \sin \theta_{w}, \quad z^{\prime}=z$
and the relation between the original image coordinates $(u, v)$ and the resulting ones ( $u^{\prime}, v^{\prime}$ ) may be described by:
$u^{\prime}=u \cos \theta_{w}+v \sin \theta_{w}, \quad v^{\prime}=u \sin \theta_{w}-v \cos \theta_{w}$.
Also, after this rotation, the circular shape of $W$ in the new camera coordinate system may be expressed by:
$\left(x^{\prime}-x_{w}^{\prime}\right)^{2}+\left(y^{\prime}-y_{w}^{\prime}\right)^{2}=R_{w}^{2}, \quad z^{\prime}=z_{w}^{\prime}$,
given that the center point $P_{w}$ of $W$ is located at $\left(x_{w}^{\prime}, y_{w}^{\prime}, z_{w}^{\prime}\right)$ with $x_{w}^{\prime}=x_{w} \cos \theta_{w}+y_{w} \sin \theta_{w}, y_{w}^{\prime}=x_{w} \sin \theta_{w}-y_{w} \cos \theta_{w}, z_{w}^{\prime}=$ $z_{w}$ according to (4). Notice that $y_{w}^{\prime}$ is now zero after the rotation according to Fig. 3, so that the above equation becomes

$$
\begin{equation*}
\left(x^{\prime}-x_{w}^{\prime}\right)^{2}+y^{\prime 2}=R_{w}^{2}, \quad z^{\prime}=z_{w}^{\prime} \tag{6}
\end{equation*}
$$

Also, by the optical geometry of the camera described by (2), we have
$\frac{v^{\prime}}{u^{\prime}}=\frac{y^{\prime}}{x^{\prime}}$,
or equivalently,
$v^{\prime}=\frac{u^{\prime}}{x^{\prime}} y^{\prime}$.
Equation (8) will be used in Section 3.1.
We are now ready to prove the previously-mentioned fact that the irregular shape of the circular landmark $W$ appearing in the omni-directional image may be well approximated by an ellipse. After horizontally rotating the camera and the image coordinate systems for the angle of $\theta_{w}=\tan ^{-1}\left(y_{w} / x_{w}\right)$ described by Eq. (3), (2) becomes

$$
\begin{align*}
u^{\prime} & =\frac{x^{\prime} f\left(b^{2}-c^{2}\right)}{\left(b^{2}+c^{2}\right)\left(z^{\prime}-c\right)-2 b c \sqrt{\left(z^{\prime}-c\right)^{2}+{x^{\prime 2}+y^{\prime 2}}^{2}}} \\
v^{\prime} & =\frac{y^{\prime} f\left(b^{2}-c^{2}\right)}{\left(b^{2}+c^{2}\right)\left(z^{\prime}-c\right)-2 b c \sqrt{\left(z^{\prime}-c\right)^{2}+{x^{\prime 2}+y^{\prime 2}}_{2}^{2}}} . \tag{2A}
\end{align*}
$$

In addition, the new $y$-coordinates $y_{w}^{\prime}$ of the landmark circle center is 0 . Then, by assuming that the horizontal distance from the origin of the camera coordinate system to the landmark is much larger than the radius of the landmark, we have $y^{\prime} \ll x^{\prime}$ and the circle $\left(x^{\prime}-x_{w}^{\prime}\right)^{2}+\left(y^{\prime}-y_{w}^{\prime}\right)^{2}=R_{w}^{2}$ with $y_{w}^{\prime}=0$ may be regarded relatively as a point which is its center located at ( $x_{w}^{\prime}, y_{w}^{\prime}$ ) so that ${x^{\prime}}^{2}+{y^{\prime 2}}^{2}{x_{w}^{\prime 2}+y_{w}^{\prime 2}=x_{w}^{\prime 2} \text {. Also, } z^{\prime} \text { is a constant (denoted as } h_{w} \text { now) }}^{2}$. because the ceiling on which the landmark is attached is assume to be parallel with the camera coordinate system. As a consequence, the second equation in (2A) above for $v^{\prime}$ can be simplified to

$$
v^{\prime}=\frac{y^{\prime} f\left(b^{2}-c^{2}\right)}{\left(b^{2}+c^{2}\right)(z-c)-2 b c \sqrt{(z-c)^{2}+x_{w}^{\prime 2}}}
$$

or equivalently,
$y^{\prime}=v^{\prime} M$
where $M$ is
$M=\frac{f\left(b^{2}-c^{2}\right)}{\left(b^{2}+c^{2}\right)(z-c)-2 b c \sqrt{(z-c)^{2}+x_{w}^{\prime 2}}}$.
The other coordinate $u^{\prime}$ of each shape pixel of the landmark $W$ may also be derived by approximation, but in a different way. Under the same assumption mentioned above that the radius of the landmark is relatively very small with respect to the horizontal distance from the origin of the camera coordinate system to the landmark, the magnitude of $x^{\prime}$ of each shape pixel of the circular landmark $W$ in the camera coordinate system is much larger than that of $y^{\prime}$. Therefore, we may neglect the influence of the magnitude of $y^{\prime}$ in the computation of $u^{\prime}$ described by the first equation in (2A) so that
$u^{\prime}=\frac{x^{\prime} f\left(b^{2}-c^{2}\right)}{\left(b^{2}+c^{2}\right)(z-c)-2 b c \sqrt{(z-c)^{2}+x^{\prime 2}}}$
and compute $u^{\prime}$ just in terms of $x^{\prime}$. Regarding the above equation in the form $u^{\prime}=F\left(x^{\prime}\right)$, we may use the Taylor series to expand the function around $x_{w}^{\prime}$ as

$$
\begin{aligned}
u^{\prime}= & F\left(x^{\prime}\right)=F\left(x_{w}^{\prime}\right)+\left[\left(x^{\prime}-x_{w}^{\prime}\right) / 1!\right] F^{\prime}\left(x_{w}^{\prime}\right) \\
& +\left[\left(x^{\prime}-x_{w}^{\prime}\right)^{2} / 2!\right] F^{\prime \prime}\left(x_{w}^{\prime}\right)+\cdots .
\end{aligned}
$$

Ignoring the terms after the second, we have
$u^{\prime} \approx F\left(x_{w}^{\prime}\right)+\left[\left(x^{\prime}-x_{w}^{\prime}\right) / 1!\right] F^{\prime}\left(x_{w}^{\prime}\right)=u_{w}^{\prime}+\left(x^{\prime}-x_{w}^{\prime}\right) F^{\prime}\left(x_{w}^{\prime}\right)$.
Equation (10) may be transformed easily into
$x^{\prime} \approx x_{w}^{\prime}+\left(u^{\prime}-u_{w}^{\prime}\right) / F^{\prime}\left(x_{w}^{\prime}\right)$
with the first derivative $F^{\prime}$ calculated to be:
$F^{\prime}\left(x_{w}^{\prime}\right)=A_{E}\left(\frac{1}{B_{E}}-\frac{C_{E} x_{w}^{\prime}}{B_{E}^{2} \sqrt{D_{E}+x_{w}^{\prime}}}\right)$,
where
$A_{E}=f\left(b^{2}-c^{2}\right)$,
$B_{E}=\left(b^{2}+c^{2}\right)(z-c)-c \sqrt{D+x_{w}^{\prime 2}}$,
$C_{E}=2 b c$,
$D_{E}=(z-c)^{2}$,
$z=h_{w}$.
Now with $x^{\prime}$ and $y^{\prime}$ available, we come to the final stage of the derivation of the equation of the ellipse for approximating the distorted circular shape of the landmark in the omni-directional image. By substituting Eqs. (9) and (11) into Eq. (6) and rearranging the result, we can get
$\frac{\left(u^{\prime}-u_{w}^{\prime}\right)^{2}}{R_{w}^{2} F^{\prime}\left(x_{w}^{\prime}\right)^{2}}+\frac{v^{\prime^{2}} M^{2}}{R_{w}^{2}}=1$
which obviously specifies exactly an elliptical shape centered at $\left(u_{w}^{\prime}, 0\right)$ with the lengths of the major and minor axes being $R_{w} F^{\prime}\left(x_{w}^{\prime}\right)$ and $R_{w} / M$, respectively. This completes the proof.

### 2.2. Effectiveness of shape approximation

To check the effectiveness of the approximation of the circular shape of the landmark by the elliptical shape using Eq. (13), we show in Fig. 4 an example of the simulation results obtained in this study, in which both the original circular shape and the approximating elliptical one are drawn and superimposed on each


Fig. 4. Simulation of a series of circular shapes of the landmark at different places, showing that the distorted landmark shape may be approximated well by ellipses. White pixels are simulated landmark shape points and black pixels are approximate ellipse points computed by Eq. (13). (a): illustration of the simulation results. (b): partially enlarged view of (a).
other for comparison: the former shape being drawn by Eq. (6) and then projected into the image plane by Eq. (2), and the latter being drawn directly by Eq. (13). The outer big circle in the figure marks the field of view of the camera. Inside the big circle, the original distorted circular shapes of $W$ at different positions are drawn with white pixels, and the approximate elliptical shapes are computed using the coordinates of the white pixels and drawn by black pixels.

From the figure, we can see that each black ellipse overlaps the corresponding white distorted circle quite well. This shows that the distorted circular shape of the landmark in the omnidirectional image indeed may be approximated by the ellipse described by Eq. (13). This discovery offers great helps, as found in this study, in utilizing this kind of circular landmark to provide the location information for vehicle guidance, as described in the following section.

## 3. Vehicle location estimation

In this section we describe the proposed method for vehicle location estimation using the detected landmark as a known reference point. From each acquired image of the ceiling, we extract the circular landmark shape by image processing techniques, including thresholding, edge detection, and ellipse detection. For thresholding, since the artificially-made circularshaped landmark contrasts well with the background in the image, a threshold value is selected to segment the distorted circular shape of the landmark in the image. And for edge detection in the image, the Sobel edge detector is applied. Since the landmark shape in the image can be regarded as an ellipse according to Section 2, an ellipse detection algorithm [10] is employed to extract the landmark, yielding an approximating ellipse with its axis lengths computed.

### 3.1. Vehicle location estimation by axis lengths of an ellipse

We will derive here the location of the landmark, including its distance and orientation, with respect to the camera coordinate system on the vehicle for use in vehicle guidance. We derive first


Fig. 5. Top view from the $z$ direction illustrating the relation between the axes of the approximating ellipse and the horizontal distance of the circular-shaped landmark.
the horizontal distance of the landmark in terms of the lengths of the two axes of the approximating ellipse. As depicted in Fig. 3, the $x^{\prime}$ axis is directed to the landmark center $P_{w}^{\prime}$. For a better view of the involved situation, Fig. 3 is redrawn as Fig. 5 in which $d$ is the horizontal distance between the camera and the center of the landmark $W$ to be derived; $P_{\alpha}^{\prime} P_{\beta}^{\prime}$ is a diameter of $W$ perpendicular to the $x^{\prime}$ axis; point $I_{\alpha}^{\prime}$ is the image of point $P_{\alpha}^{\prime}$; and point $I_{\beta}^{\prime}$ is the image of point $P_{\beta}^{\prime}$. It follows from Eq. (7) that
$\frac{v_{\alpha}^{\prime}}{u_{\alpha}^{\prime}}=\frac{y_{\alpha}^{\prime}}{x_{\alpha}^{\prime}}$
where ( $u_{\alpha}^{\prime}, v_{\alpha}^{\prime}$ ) are the coordinates of $I_{\alpha}^{\prime}$ in the ( $u^{\prime}, v^{\prime}$ ) coordinate system and $\left(x_{\alpha}^{\prime}, y_{\alpha}^{\prime}\right)$ are the coordinates of $P_{\alpha}^{\prime}$ in the ( $x^{\prime}, y^{\prime}$ ) coordinate system. Similarly, we have
$\frac{v_{\beta^{\prime}}}{u_{\beta}^{\prime}}=\frac{y_{\beta^{\prime}}}{x_{\beta^{\prime}}}$
where ( $u_{\beta}^{\prime}, v_{\beta}^{\prime}$ ) are the coordinates of $I_{\beta}^{\prime}$ in the ( $u^{\prime}, v^{\prime}$ ) coordinate system and $\left(x_{\beta}^{\prime}, y_{\beta}^{\prime}\right)$ are the coordinates of $P_{\beta}^{\prime}$ in the ( $x^{\prime}, y^{\prime}$ ) coordinate system. Since $\overline{P_{\alpha}^{\prime P_{\beta}^{\prime}}}$ is the diameter of $W$ perpendicular to the $x^{\prime}$ axis, we have $x_{\alpha}^{\prime}=x_{\beta}^{\prime}$ and so $u_{\alpha}^{\prime}=u_{\beta}^{\prime}$. Therefore, Eqs. (14) and (15) can be merged and rearranged to result in
$\frac{v_{\alpha}^{\prime}-v_{\beta}^{\prime}}{u_{\alpha}^{\prime}}=\frac{y_{\alpha}^{\prime}-y_{\beta}^{\prime}}{x_{\alpha}^{\prime}}$
where $y_{\alpha}^{\prime}-y_{\beta}^{\prime}$ is the length of $\overline{P_{\alpha}^{\prime} P_{\beta}^{\prime}}$ (denoted as $\left\|\overline{P_{\alpha}^{\prime} P_{\beta}^{\prime}}\right\|$ ) which is the known in advance; $v_{\alpha}^{\prime}-v_{\beta}^{\prime}$ is the length of $\overline{I_{\alpha}^{\prime} I_{\beta}^{\prime}}$ (denoted as $\left.\left\|\overline{I_{\alpha}^{\prime} I_{\beta}^{\prime}}\right\|\right)$ which is the major axis of the approximating ellipse in the image plane; and $u_{\alpha}^{\prime}$ is the $u^{\prime}$ coordinate of the center of the ellipse. The latter two parameters $\left\|\overline{I_{\alpha}^{\prime} I_{\beta}^{\prime}}\right\|$ and $u_{\alpha}^{\prime}$ can be computed right after the approximating ellipse is obtained. Also, as seen from the figure, $x_{\alpha}^{\prime}$ is just the desired relative horizontal distance $d$ between the camera and the center of the landmark $W$, or equivalently, the desired horizontal distance $d$ of the landmark with respect to the vehicle. Therefore, we can derive from Eq. (16) the desired value of $d$ as
$d=\frac{\left\|\overline{P_{\alpha}^{\prime} P_{\beta}^{\prime}}\right\|}{\left\|\overline{I_{\alpha}^{\prime} I_{\beta}^{\prime}}\right\|} \times u_{\alpha}^{\prime}$.
Furthermore, using the ellipse makes it easier to solve the orientation $\theta_{w}$ of the landmark with respect to the camera
coordinate system, or equivalently, with respective to the vehicle. Given that the center of the found ellipse in the image is located at ( $u_{w}, v_{w}$ ), from Eq. (3) and the following equation derived from Eq. (7),
$\frac{y_{w}}{x_{w}}=\frac{v_{w}}{u_{w}}$,
we can calculate $\theta_{w}$ by
$\theta_{w}=\tan ^{-1}\left(\frac{y_{w}}{x_{w}}\right)=\tan ^{-1}\left(\frac{v_{w}}{u_{w}}\right)$.
A merit of the above procedure is that there is no need of the vertical height value $z_{w}$ of the landmark with respect to the camera coordinate system in computing the distance $d$ and the orientation $\theta_{w}$ of the landmark. This provides an advantage of allowing dynamic changes of the camera height for the purpose of avoiding camera view occlusion by surrounding people or objects. Taking this advantage, we have included a shaft in the vehicle system for adjusting the height of the camera dynamically: if the landmark shape cannot be well extracted from the image taken at a certain camera height to yield an approximating ellipse, then the camera is lifted up automatically and gradually until a good result is obtained.

Another merit of vehicle location estimation by Eqs. (17) and (18) is that the exact hyperbolic mirror shape of the omnidirectional camera, as described in Eq. (1), need not be considered. This reduces the estimation error caused by using the possibly imprecise shape parameters of the mirror obtained by calibration, and simplifies the computation process involved in the estimation. Also, it provides a nature of generality of the proposed location estimation process using a given type of camera, so that it is unnecessary to re-design the location estimation process when a camera with a different hyperbolic mirror shape is used.

### 3.2. Estimation of vehicle move distances and orientation changes

In the previous section, we show how to estimate the distance and orientation of the landmark with respect to the vehicle. In this section we show how to find out, as an application of the previous results, the relative distance and orientation of the vehicle in a navigation cycle with respect to its location in the previous cycle, which we call the move distance and orientation change of the vehicle, respectively. Derivations of these parameters are useful for a number of autonomous vehicle applications, including recording of navigation paths, path planning for vehicle guidance, measurement of guidance errors, etc.

As shown in Fig. 6(a) and (b), we denote the move distance of the vehicle between two consecutive observation times $T_{1}$ and $T_{2}$ as $D$. Using the approximating ellipse, we can, according to Section 3.1, calculate the horizontal distances $d_{1}, d_{2}$ and the orientations $\theta_{1}, \theta_{2}$ of the landmark at $T_{1}$ and $T_{2}$, respectively, with respect to the vehicle. Based on the cosine theorem, we have
$d_{1}^{2}+D^{2}-2 d_{1} \times D \times \cos \theta_{1}=d_{2}^{2}$,
which may be solved to get the desired move distance $D$ as
$D=d_{1} \cos \theta_{1}-\sqrt{d_{1}^{2} \cos ^{2} \theta_{1}-d_{1}^{2}+d_{2}^{2}}$ if $\theta_{2} \leq 90^{\circ}$; or
$D=d_{1} \cos \theta_{1}+\sqrt{d_{1}^{2} \cos ^{2} \theta_{1}-d_{1}^{2}+d_{2}^{2}} \quad$ if $\theta_{2}>90^{\circ}$.
Next, to find the desired orientation change of the vehicle, which we denote as $\gamma$, caused by a vehicle turning between the two consecutive observations, we acquire first, using Eq. (18), the orientations of the landmark with respect to the vehicle before and after the vehicle turning, denoted as $\theta_{2}$ and $\phi$, respectively, as depicted in Fig. 7(c) and (d). Then, $\gamma$ can be computed easily by
$\gamma=\theta_{2}-\phi$.


Fig. 6. Illustration of the relative ALV location estimation. (a) and (b): the displacement $D$ of the vehicle. (c) and (d): the orientation of the vehicle.

## 4. Experimental results

The effectiveness of the proposed location estimation method has been tested by some experiments conducted in this study, which include two parts: (1) using computer simulations to test if the circular shape of the landmark in the acquired images taken with omni-directional cameras with different shapes of hyperboloidal mirrors can be detected by the proposed ellipse approximation method; (2) using real images to determine the precision of the estimated vehicle locations relative to the landmark.

### 4.1. Simulations

In the first experiment of landmark shape approximation by ellipses, the first step was to create landmark shapes at different locations. A series of virtual circular-shaped landmarks with a radius of 20 cm were created and projected onto the image plane, in which the centers of these landmarks are located in a range of 300 cm in intervals of 50 cm with the orientation angles $\theta$ ranging from $0^{\circ}$ to $360^{\circ}$ in intervals of $5^{\circ}$. Two kinds of common distortion, barrel and pincushion distortion as described in [11, 12], were added to make the simulation more realistic. In our simulations, the original image coordinates $(u, v)$ are inherently normal and distortion-free, as described by Eq. (2).

Then, we add barrel and pincushion distortion to them by the following equations:
$\breve{u}=u+u\left[k_{1}\left(u^{2}+v^{2}\right)+k_{2}\left(u^{2}+v^{2}\right)^{2}\right] ;$
$\breve{v}=v+v\left[k_{1}\left(u^{2}+v^{2}\right)+k_{2}\left(u^{2}+v^{2}\right)^{2}\right]$
where $(\breve{u}, \breve{v})$ are the distorted image coordinates, and $k_{1}$ and $k_{2}$ are two parameters to control the shape of the geometric distortion. The coordinates $(\breve{u}, \breve{v})$ then are taken as input to our method.

Second, an ellipse detection algorithm [10] was used to detect these landmarks. Third, a rate of successful ellipse detections was computed. And at last, the three steps were repeated to compute the rates of successful ellipse detections for different kinds of omni-directional cameras which were created virtually only by changing the parameters of their hyperboloidal mirrors. More specifically, we changed only the mirror parameter $b$ in (1) while maintaining the value of $c$ invariant $(=20 \mathrm{~mm}$ in our simulations) since the position and the focus of the cameras need not be changed. The smallest value of $b$ was taken to be 146 mm

Table 1
Rates of successful detections of landmark shapes taken by cameras with different shapes of hyperboloidal reflection mirror ( $c=20 \mathrm{~mm}$ ).

| $b$ (unit mm) | Detection rate (\%) |
| :--- | :--- |
| 146 | 100 |
| 147 | 100 |
| 148 | 100 |
| 149 | 100 |
| 150 | 100 |
| 151 | 100 |
| 152 | 100 |
| 153 | 100 |
| 154 | 100 |
| 155 | 100 |
| 157 | 100 |
| 158 | 100 |
| 159 | 95 |

since otherwise the landmark image will exceed the range of the image plane. And the largest value of $b$ was taken to be 158 mm because otherwise the rate of successful ellipse detection will drop dramatically owing to the shrinking of the landmark shape to a point in the image. The results are shown in Table 1. Examples of successful detections of ellipses in both original and distorted images are shown in Fig. 7.

The simulation shows that the lens distortion has only a minor influence on the landmark detection. As indicated by Table 1, given shapes with proper sizes and reasonable image distortions such as the examples shown in Fig. 7, almost all landmarks can be successfully detected from the omni-directional images, even when the images are taken with cameras with different hyperboloidal mirrors.

### 4.2. Experimental results of real images for vehicle location estimation

The proposed method was also applied to two sets of real images. As shown in Fig. 8, both sets of images were taken with an upward-looking omni-directional camera mounted on an expandable vertical shaft on an autonomous vehicle. The relative positions of the camera, ceiling, and landmark are illustrated in Fig. 1. When performing location estimation, the shaft was lifted to raise the camera to the height of 1.4 m . Then, a landmark with a radius of 40 cm attached on the ceiling with a height of 2.9 m from the ground was imaged and its shape in the image detected. All


Fig. 7. Examples of successful detection of elliptical shapes. In (a)-(f), the elliptical shapes of simulated landmark images are marked by white pixels. Black pixels are approximate ellipse points computed by the ellipse detection algorithm [10]. In (b)-(f), both horizontal and vertical grid lines are added in order to indicate the level of geometric distortion in each simulated image.
the images in the first set were taken from an identical orientation but with different distances from the camera to the landmark for the purpose of investigating the relation between the landmark distance and the estimation error. The results of this experiment are shown in Table 2. All the images in the second set such as those shown in Fig. 9 were taken from an identical orientation and at an identical location but with different camera heights for the purpose of investigating the relation between the depth variation with respect to the estimation. For measurement of the estimation precision, we define a distance error ratio and an orientation error as follows:

## distance error ratio

$=($ real distance - estimated distance $) /($ real distance $) ;$
orientation error $=$ real orientation - estimated orientation.
The distance error ratios and orientation errors computed from the two sets of images are shown in Tables 2 and 3, respectively. The resolution of image is 640 by 480 . The number of times of
experiments is five, that is, each distance or orientation value in Tables Tables 2 and 3 is the average of the data measured from the same orientation for five times. From the tables, we see that all the distance error ratios are smaller than $5 \%$ and that all the orientation errors are smaller than $2^{\circ}$. Such estimation precisions are sufficient for the purpose of autonomous vehicle guidance and navigation purposes.

### 4.3. Identification and arrangement of the proposed landmarks in real applications

With a consideration of the integrity of a landmark-based navigation system, solving the identification and arrangement problems of the proposed landmarks is inevitable for our system. For example, how does the robot identify some landmark at which it is looking at a certain moment if it was taught the arrangement of landmarks in advance? In this section, we will discuss the identification and arrangement of the proposed landmarks in real applications.


Fig. 8. All the experimental images were taken by an autonomous land vehicle equipped with an upward-looking omni-directional camera. (a): the autonomous land vehicle. (b): a close look of the camera on the vehicle.


Fig. 9. Two example images acquired by the camera equipped on the vehicle. (a) and (c): images acquired at different positions. (b) and (d): the enlarged images of the landmarks in (a) and (c), respectively.

Table 2
Error ratios in location estimations with landmarks located in the same directions but at different distances.

| Estimated distance: $d$ | Real distance: $d$ | Estimated orientation | Real orientation | Distance error ratio (\%) | Orientation error (degree) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 0.985 | 1.000 | -80.8 | -81.5 | 1.5 | 0.7 |
| 1.474 | 1.500 | -81.4 | -81.5 | 1.7 | 0.2 |
| 1.959 | 2.000 | -83.0 | -81.5 | 2.0 | 1.5 |
| 2.440 | 2.500 | -83.0 | -81.5 | 2.4 | 1.5 |
| 2.925 | 3.000 | -82.8 | -81.5 | 2.5 | 1.3 |
| 3.384 | 3.500 | -81.7 | -81.5 | 0.3 | 0.2 |
| 3.862 | 4.000 | -80.9 | -81.5 | 3.5 | 0.6 |
| 4.359 | 4.500 | -81.6 | -81.5 | 3.1 | 0.1 |
| 4.859 | 5.000 | -81.1 | -81.5 | 2.8 | 0.4 |
| 5.281 | 5.500 | -81.6 | -81.5 | 4.0 | 0.1 |
| 5.801 | 6.000 | -81.8 | -81.5 | 3.3 | 0.3 |
| 6.212 | 6.500 | -81.1 | -81.5 | 4.4 | 0.4 |

Table 3
Errors in location estimations with the landmarks located in the same directions and at the same distances but with different camera heights.

| Height of landmark from camera <br> $(\mathrm{m})$ | Estimated <br> distance: $d$ | Real <br> distance: $d$ | Estimated <br> orientation | Real <br> orientation | Distance error <br> ratio $(\%)$ | Orientation error $($ degree $)$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 2.5 | 3.076 | 3.000 | -43.5 | -42 | 2.5 | -1.5 |
| 2.25 | 3.032 | 3.000 | -44.2 | -42 | 1.1 | -2.2 |
| 2 | 3.074 | 3.000 | -43.802 | -42 | 2.5 | -1.802 |
| 1.75 | 3.039 | 3.000 | -41.845 | -42 | 0.155 |  |
| 1.5 | 3.051 | 3.000 | -40.569 | -42 | 1.3 | 1.431 |
| 1.25 | 3.097 | 3.000 | -42.466 | -42 | 3.2 | -0.466 |
| 1 | 2.942 | 3.000 | -41.388 | -42 | -1.9 | 0.612 |



Fig. 10. Coloring scheme for identification of multiple circular shapes.
We solve the identification problem of individual landmarks by creating a color coding system. Each landmark is colored by two colors forming two concentric circles with each color being with one of nine pre-selected colors, as illustrated in Fig. 10. Furthermore, the nine colors are equally spaced in the hue attribute of the HSI color system, in order to make them more separable and reduce the influence of the lighting condition. Consequently, there are 81 different color combinations for use as the identification numbers to differentiate the landmarks in the map.

Moreover, since the location accuracy using our method becomes worse than $4 \%$ at distances of about 5 m , we suggest repeating the circular landmark on the ceiling at intervals of 10 m . Also, the repetitions should be done in two dimensions, forming a pattern of square grids with 10 m sides. The diameter of the circular landmark is 80 cm for a ceiling at a height of 2.9 m . If the ceiling height is changed, then the size of the circle may be changed proportionally.

## 5. Conclusion

In this study, a new approach to location estimation of an autonomous vehicle for navigation guidance in an indoor environment using a circular-shaped landmark on the ceiling by omni-directional vision techniques has been proposed. It is proved both by theoretical derivations and experimental results that the distorted landmark shape appearing in the image may
be well approximated, based on the application of Taylor series expansion, by an ellipse. After the elliptical shape is extracted by an ellipse extraction algorithm, a location estimation approach is proposed by using the ellipse parameters for autonomous vehicle applications.

The proposed location estimation approach with a unique ability of allowing dynamic camera height changes increases the flexibility of creating an occlusion-free camera view in unknown complex environments with obstacles. Additionally, the exact hyperbolic mirror shape of the omni-directional camera need not be considered which reduces the estimation error caused by the use of the imprecise shape parameters of the mirror obtained from calibration. The computation of the proposed approach is analytic, thus speeding up the estimation process and so reducing the navigation cycle time. Both simulated and real images were tested and good experimental results prove the effectiveness of the proposed approach.

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