

Modeling with High-Order Differential Equations



National Chiao Tung University

Chun-Jen Tsai

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Linear Models: IVP

- Many linear dynamic systems can be represented using a 2nd order DE with constant coefficients:

$$a_2 \frac{d^2 y}{dt^2} + a_1 \frac{dy}{dt} + a_0 y = g(t)$$

In this formulation, $g(t)$ is the input or forcing function of the system, the output of the system is a solution $y(t)$ of the DE that satisfies the initial conditions $y(t_0) = y_0, y'(t_0) = y_1$ on an interval containing t_0 .

Free Undamped Motion

- Hooke's law describes the restoring force:

$$F = ks$$

- Newton's 2nd law ($F = ma$) describes the motion:

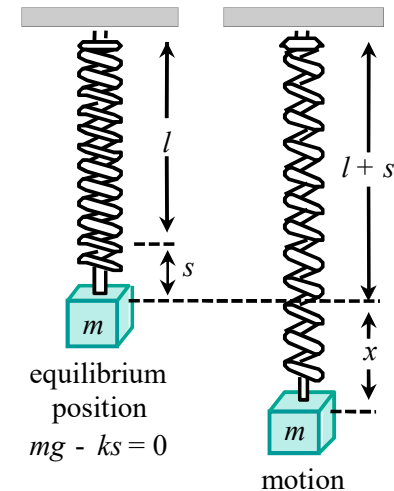
$$\begin{aligned} m(d^2x/dt^2) &= -k(s + x) + mg \\ &= -kx + (mg - ks) = -kx \end{aligned}$$

- DE of free undamped motion:

$$\frac{d^2x}{dt^2} + \omega^2 x = 0, \quad x(0) = x_0, \quad x'(0) = x_1$$

- Solution of the motion:

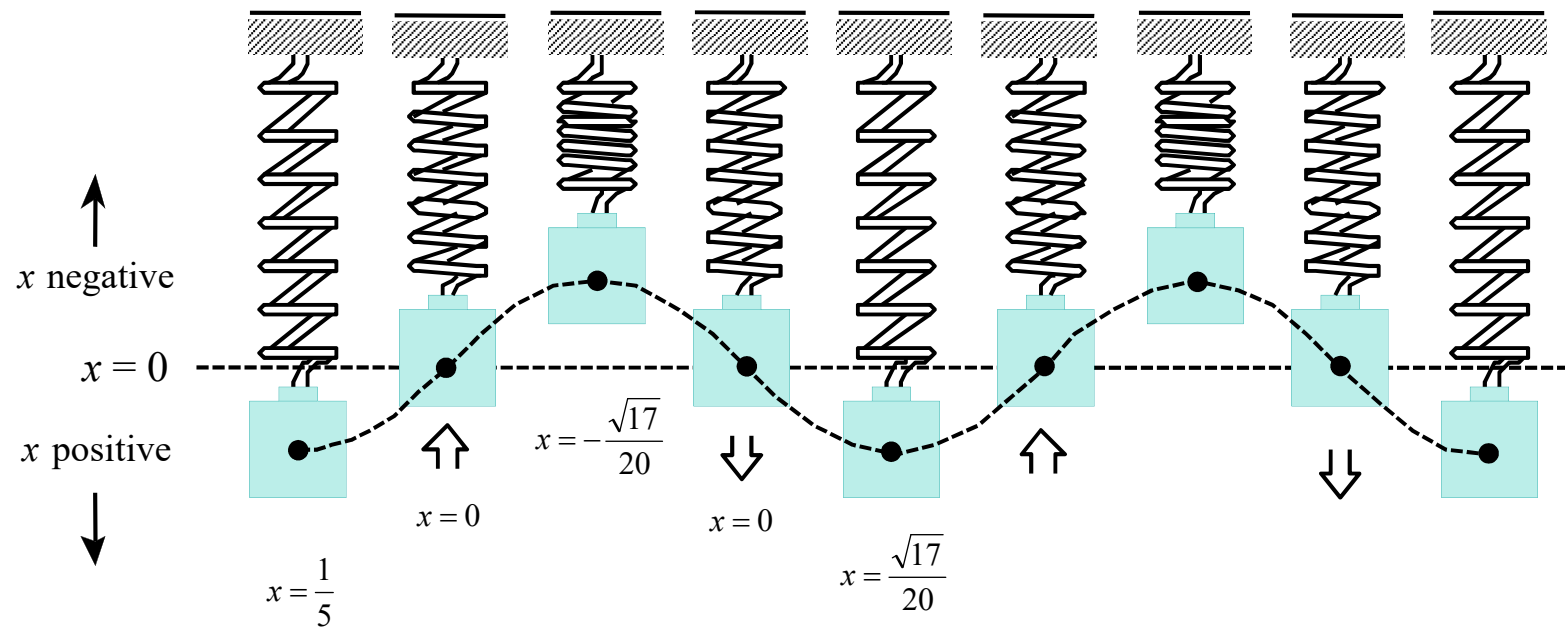
$$x(t) = c_1 \cos \omega t + c_2 \sin \omega t.$$



Alternative Form of Solution

- By applying trigonometric formula, we have:

$$x(t) = A \sin(\omega t + \phi), \quad A = \sqrt{c_1^2 + c_2^2}, \quad \tan \phi = \frac{c_1}{c_2}$$



Aging Spring

- In real world, the spring constant k usually varies as the spring gets old. Replace k with $k(t) = ke^{-\alpha t}$, $k > 0$, $\alpha > 0$, we have a more realistic system model:

$$mx'' + ke^{-\alpha t}x = 0$$

→ Non-constant coefficient 2nd-order linear DE!

Free Damped Motion

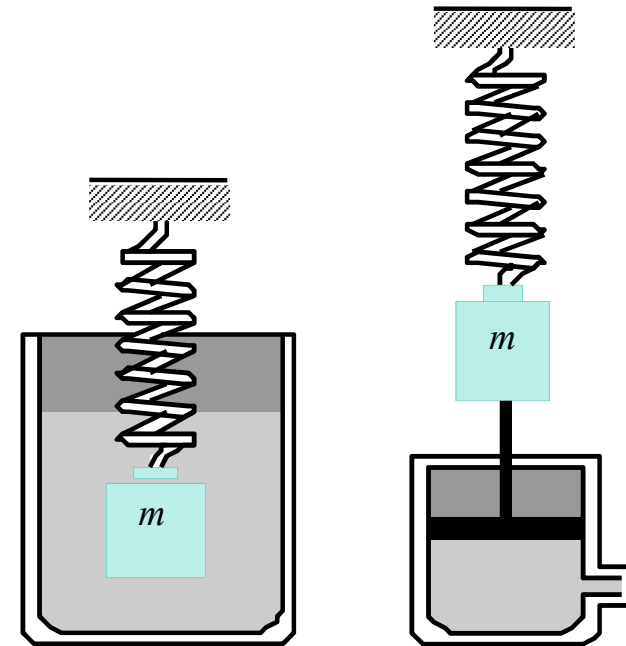
- DE of free damped motion:

$$m \frac{d^2 x}{dt^2} = -kx - \beta \frac{dx}{dt}$$

$$\rightarrow \frac{d^2 x}{dt^2} + 2\lambda \frac{dx}{dt} + \omega^2 x = 0$$

→ The roots of the auxiliary eq.:

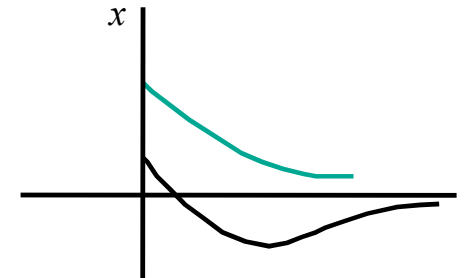
$$m = -\lambda \pm \sqrt{\lambda^2 - \omega^2}$$



Three Cases of Damped Motion

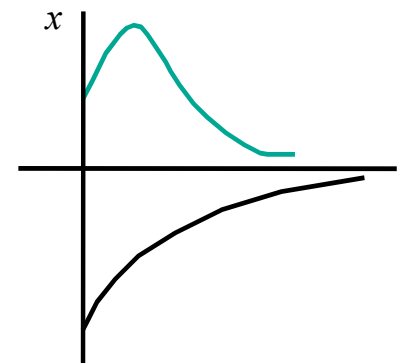
- Case I: Over-damped

$$x(t) = e^{-\lambda t} (c_1 e^{\sqrt{\lambda^2 - \omega^2} t} + c_2 e^{-\sqrt{\lambda^2 - \omega^2} t})$$



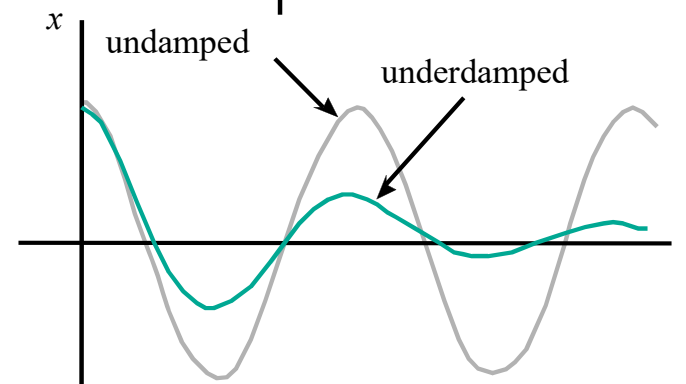
- Case II: Critically damped

$$x(t) = e^{-\lambda t} (c_1 + c_2 t)$$



- Case III: Under-damped

$$x(t) = e^{-\lambda t} (c_1 \cos \sqrt{\omega^2 - \lambda^2} t + c_2 \sin \sqrt{\omega^2 - \lambda^2} t)$$

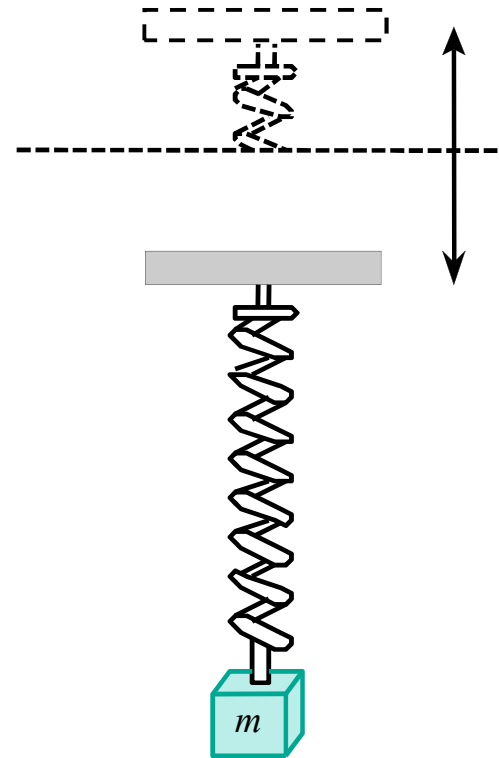


Driven Motion

- Now, consider the effect of external force $f(t)$ on the damped motion system:

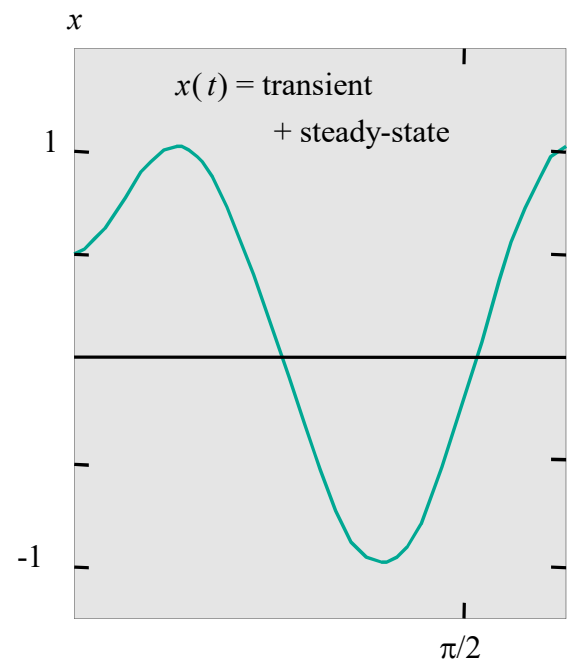
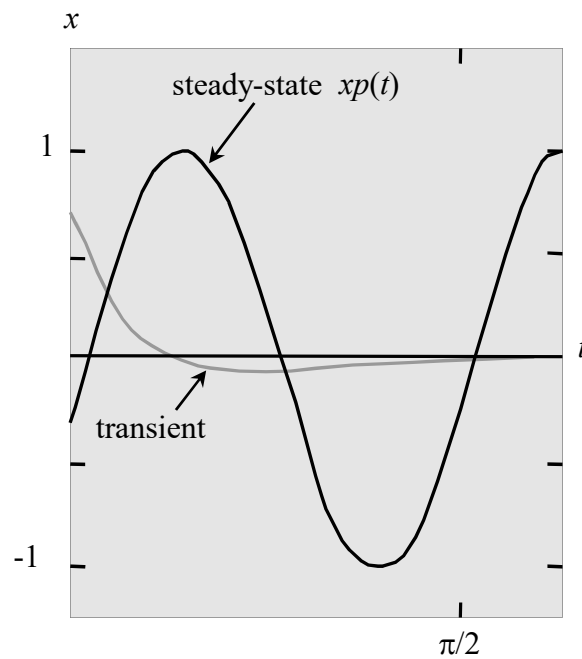
$$m \frac{d^2 x}{dt^2} = -kx - \beta \frac{dx}{dt} + f(t)$$

$$\rightarrow \frac{d^2 x}{dt^2} + 2\lambda \frac{dx}{dt} + \omega^2 x = F(t)$$



Transient and Steady-State Terms

- When $F(t)$ is a periodic function and $\lambda > 0$, the solution is the sum of a non-periodic function $x_c(t)$ and a periodic function $x_p(t)$. Moreover $\lim_{t \rightarrow \infty} x_c(t) = 0$.

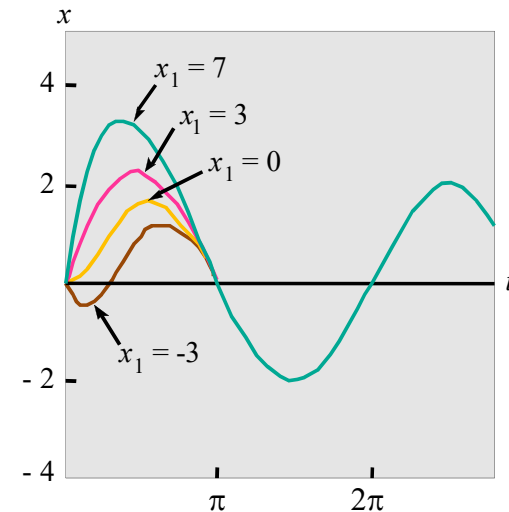


Example: Transient/Steady State

- The solution of

$$\frac{d^2x}{dt^2} + 2\frac{dx}{dt} + 2x = 4\cos t + 2\sin t, \quad x(0) = 0, \quad x'(0) = x_1$$

is $x(t) = \underbrace{(x_1 - 2)e^{-t} \sin t}_{\text{transient}} + \underbrace{2 \sin t}_{\text{steady-state}},$



Undamped Forced Motion

□ The solution of

$$\frac{d^2x}{dt^2} + \omega^2 x = F_0 \sin \gamma t, \quad x(0) = 0, \quad x'(0) = 0$$

is

$$x(t) = c_1 \cos \omega t + c_2 \sin \omega t + \frac{F_0}{\omega^2 - \gamma^2} \sin \gamma t$$

where $c_1 = 0$, $c_2 = -\gamma F_0 / \omega(\omega^2 - \gamma^2)$.

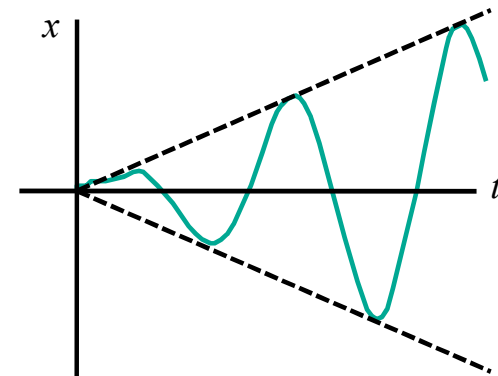
$$\rightarrow x(t) = \frac{F_0}{\omega(\omega^2 - \gamma^2)} (-\gamma \sin \omega t + \omega \sin \gamma t), \quad \gamma \neq \omega$$

→ There is no transient term.

Pure Resonance

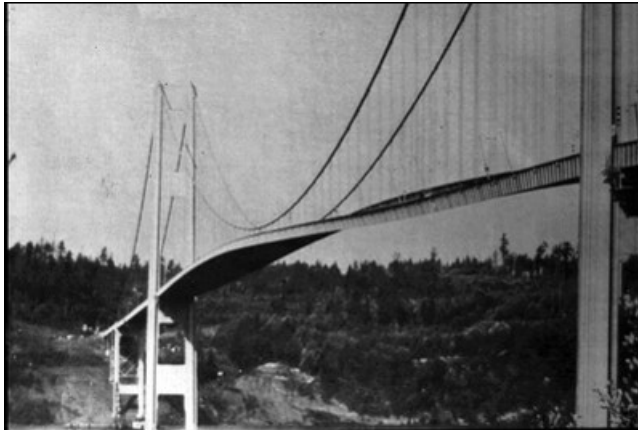
- In the previous example, when $\gamma \rightarrow \omega$, the displacement of the system become large as $t \rightarrow \infty$.

$$\begin{aligned}x(t) &= \lim_{\gamma \rightarrow \omega} F_0 \frac{-\gamma \sin \omega t + \omega \sin \gamma t}{\omega(\omega^2 - \gamma^2)} \\&= F_0 \lim_{\gamma \rightarrow \omega} \frac{\frac{d}{d\gamma}(-\gamma \sin \omega t + \omega \sin \gamma t)}{\frac{d}{d\gamma}(\omega^3 - \omega\gamma^2)} \\&= \frac{F_0}{2\omega^2} \sin \omega t - \frac{F_0}{2\omega} t \cos \omega t\end{aligned}$$



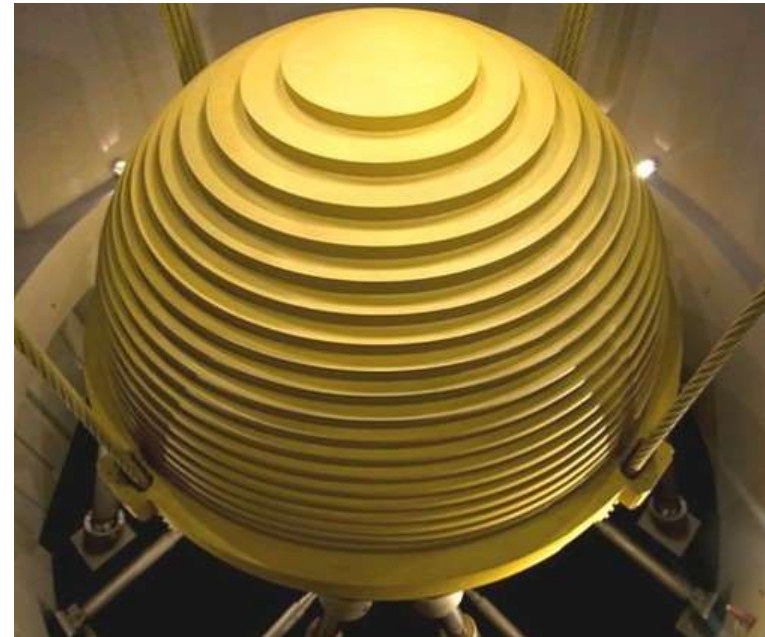
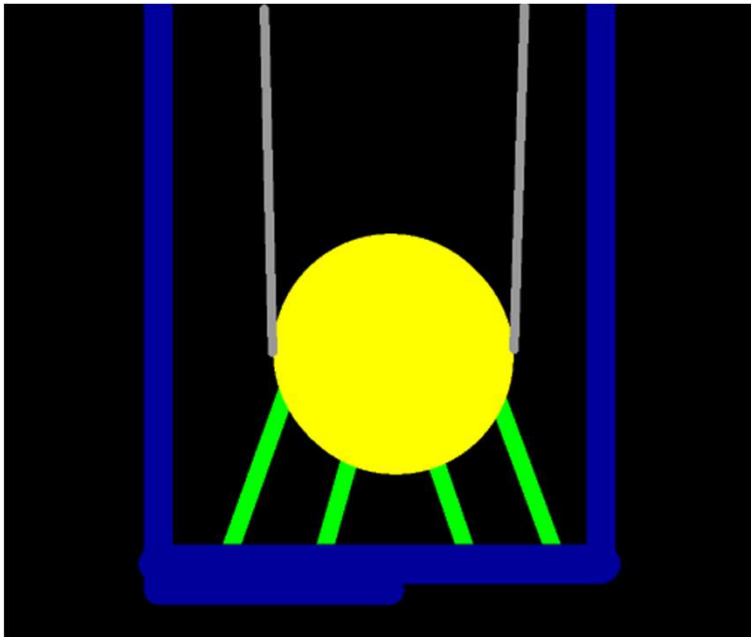
Tacoma Narrow Bridge, WA, USA

- ❑ Opened in July 1, 1940, collapsed in Nov. 7, 1940.
 - The wind-blow frequency matched the natural frequency of the bridge, which caused a pure resonance effect that destroyed the bridge.



Damping System of Taipei 101

- Taipei 101 uses a 730-ton damping ball[†] to stabilize the building under wind-blow effect



[†] Picture from: https://nl.m.wikipedia.org/wiki/Bestand:Tuned_mass_damper.gif

Linear Models: BVP

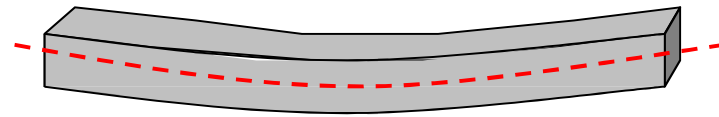
- The deflection of a flexible beam can be modelled by a 4th-order differential equation:

$$EI \frac{d^4 y}{dx^4} = w(x)$$

flexural rigidity load per unit length



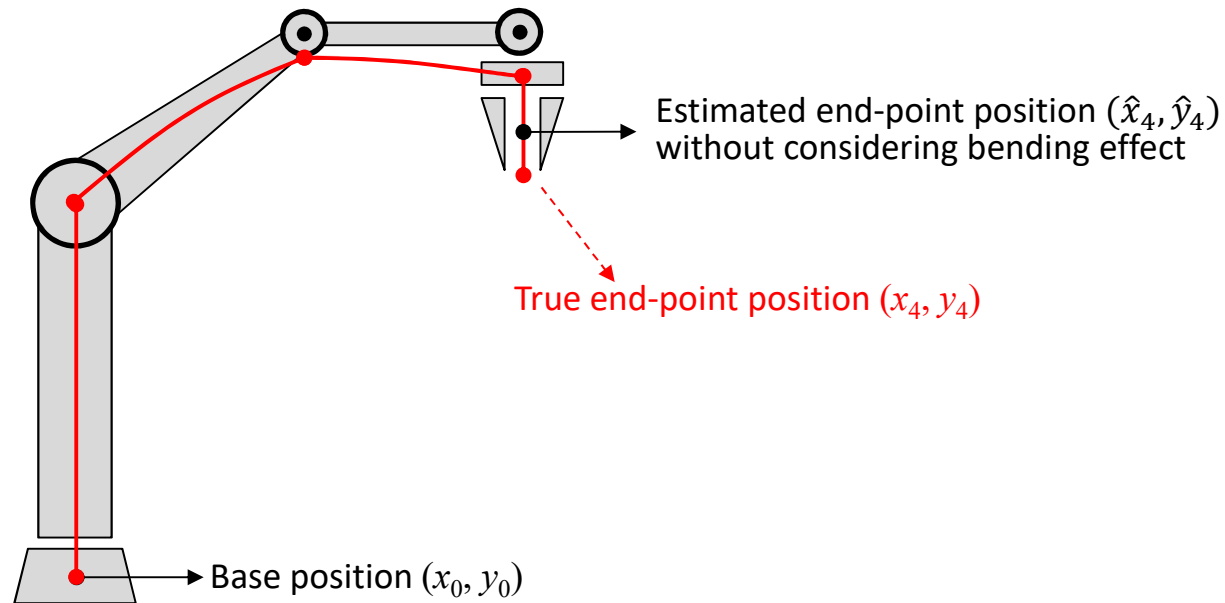
A straight flexible beam



The deflection curve of the beam

Flexible Beam Applications

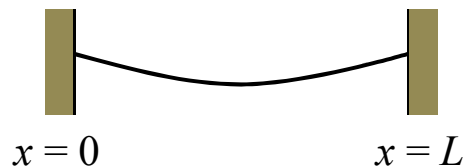
- For precise robot arm control, we must take into account the bending effect of the robot links:



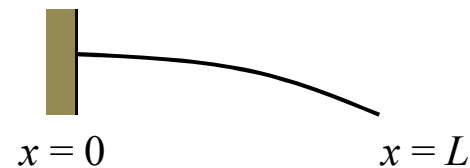
Boundary Conditions

- Boundary conditions of a flexible beam:

End of beam	Boundary conditions	
embedded	$y = 0$	$y' = 0$
free	$y'' = 0$	$y''' = 0$
supported	$y = 0$	$y'' = 0$



Embedded at both ends



Free at the right end



Supported at both ends

Eigenvalue Problems

- An eigenvalue problem in DE is a homogeneous BVP such that the boundary conditions evaluate to 0 and there is a parameter λ at the coefficient of y :

$$y'' + p(x)y' + \lambda q(x)y = 0, y(a) = 0, y(b) = 0.$$

The eigenvalue problem tries to find a λ (eigenvalue) such that the BVP has a nontrivial solution.

- The non-trivial solution that corresponding to an eigenvalue λ is then called an eigenfunction.

Example: $y'' + \lambda y = 0, y(0) = y(L) = 0$ (1/2)

- The problem can be solved by enumerating different cases when $\lambda = 0$, $\lambda < 0$, and $\lambda > 0$.

(1) $\lambda = 0$, we have $y'' = 0$,

→ the general solution is $y(x) = Ax + B$.

→ $y = 0$ is the only solution for the BVP

→ $\lambda = 0$ is not an eigenvalue of the BVP

(2) $\lambda < 0$, let $\lambda = -\alpha^2$, $\alpha > 0$, we have $y'' - \alpha^2 y = 0$,

→ the general solution is $y(x) = c_1 e^{\alpha x} + c_2 e^{-\alpha x}$.

→ $y = 0$ is the only solution for the BVP

→ $\lambda < 0$ do not have eigenvalues of the BVP

Example: $y'' + \lambda y = 0, y(0) = y(L) = 0$ (2/2)

- (3) $\lambda > 0$, let $\lambda = \alpha^2, \alpha > 0$, we have $y'' + \alpha^2 y = 0$,
→ the solution is $y(x) = c_1 \cos(\alpha x) + c_2 \sin(\alpha x)$.
→ $y(0) = 0$ implies $c_1 = 0$
→ $y(L) = 0$ implies $\sin(\alpha L) = 0$, or $\alpha L = n\pi, n \in \mathbb{Z}$
→ The BVP has infinitely many eigenvalues:

$$\lambda = \left(\frac{n\pi}{L}\right)^2, \quad n \in \mathbb{Z}$$

and the corresponding eigenfunctions are:

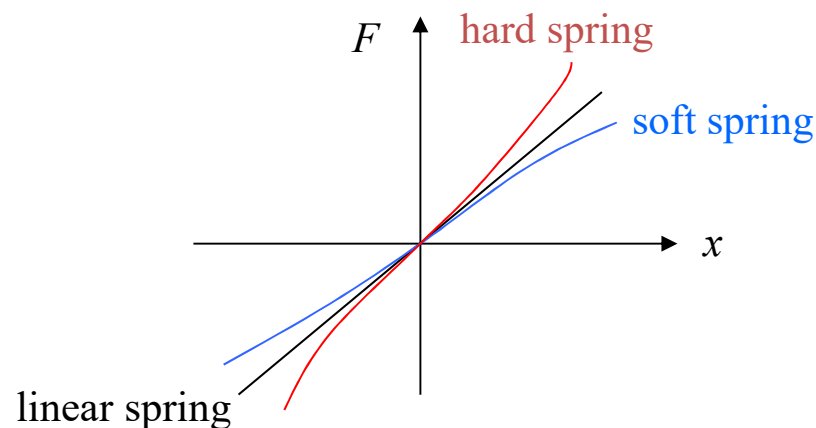
$$y_n = c_2 \sin\left(\frac{n\pi}{L}x\right), \quad n = 1, 2, 3, \dots$$

Nonlinear Spring Models (1/2)

- The general mathematical model of an undamped spring has the form:

$$m \frac{d^2 x}{dt^2} + F(x) = 0$$

for a linear spring model, $F(x) = kx$. However, springs are quite often nonlinear, e.g. $F(x) = kx + k_1x^3$.



Nonlinear Spring Models (2/2)

- Damping force of a spring system can be nonlinear as well:

$$m \frac{d^2 x}{dt^2} + \beta \left| \frac{dx}{dt} \right| \frac{dx}{dt} + F(x) = 0$$

- Restoring force $F(x)$ is usually an odd function such as $kx + k_1 x^3$. The reason is that we want $F(-x) = -F(x)$.

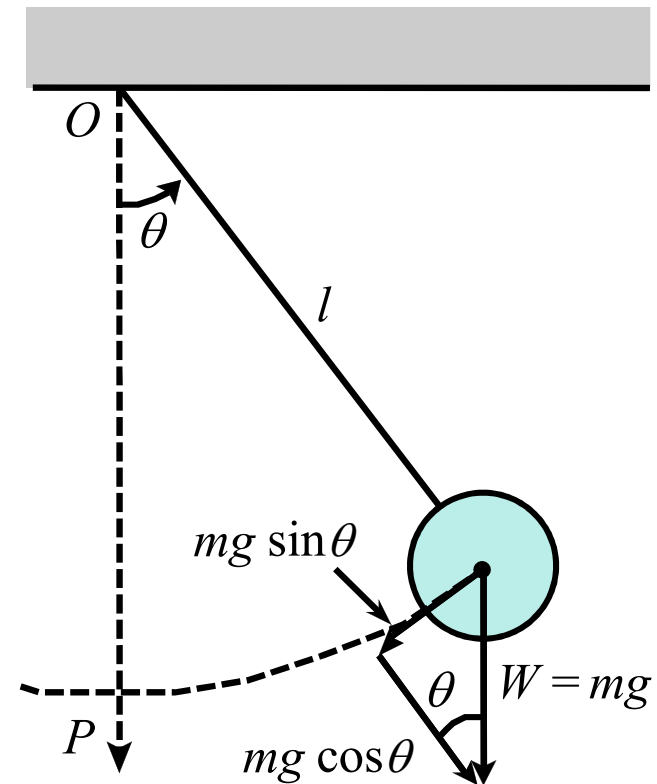
Nonlinear Pendulum

- The pendulum system can be modeled as

$$\frac{d^2\theta}{dt^2} + \frac{g}{l} \sin \theta = 0.$$

Using Maclaurin series of $\sin \theta$, we have

$$\sin \theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \dots,$$



Linearization of Nonlinear Systems

- Assuming that $\sin \theta \approx \theta - \theta^3/6$, we have:

$$\frac{d^2\theta}{dt^2} + \left(\frac{g}{l}\right)\theta + \left(\frac{g}{6l}\right)\theta^3 = 0. \quad \rightarrow \quad \text{A nonlinear model similar to the spring systems!}$$

System can be linearized by assuming $\sin \theta \approx \theta$:

$$\frac{d^2\theta}{dt^2} + \left(\frac{g}{l}\right)\theta = 0.$$

- Impact of initial values:

